Sonification of Range Information for 3D Space Perception*

Evangelos Milios¹

Bill Kapralos²

Agnieszka Kopinska ³

Sotirios Stergiopoulos²

¹ Faculty of Computer Science, Dalhousie University, Halifax, Canada, B3H 1W5

² Department of Computer Science, York University, North York, Ontario, Canada, M3J 1P3

 3 Department of Psychology, York University, North York, Ontario, Canada M3J 1P3

January 10, 2002

Abstract

We present a device that allows 3-D Space Perception by sonification of range information obtained via a point laser range sensor. The laser range sensor is worn by a blindfolded user, who scans space by pointing the laser beam in different directions. The resulting stream of range measurements is then converted to an auditory signal whose frequency or amplitude varies with the range. Our device differs from existing navigation aids for the visually impaired. Such devices use sonar ranging whose primary purpose is to detect obstacles for navigation, a task to which sonar is well suited due to its wide beam width. In contrast, the purpose of our device is to allow users to perceive the details of 3D space that surrounds them, a task to which sonar is ill suited, due to artifacts generated by multiple reflections and due to its limited range. Preliminary trials demonstrate that the user is able to easily and accurately detect corners and depth discontinuities and to perceive the size of the surrounding space.

^{*}A summary of a preliminary version of the design without experiments on human subjects was presented at the Joint ICAD/ASA/EAA Workshop on Auditory Display, March 20, 1999, Berlin, Germany.

1 Introduction

Helping the visually impaired perceive the space around them with Electronic Travel Aids (ETA) relies on providing spatial feedback via non-visual senses, primarily hearing and touch. Certain devices [7] have the ambitious goal of sonifying video images, but most are intended to facilitate navigation. Ultrasonic sensors have low cost and a wide beam width suitable for detecting obstacles in front of a visually impaired person, and have formed the basis of the majority of the devices [5, 4, 1, 2, 11]. One problem with sonar is that their resolution is not high enough for detecting drop-offs (e.g. steps down). Laser radar has been used, as well. The Talking Cane is capable not only of obstacle detection, but also of detecting reflections from bar coded retroreflecting signs, which are converted into spoken messages [6]. The Laser Cane uses range measurement by triangulation, and detects objects for two distinct elevations, and provides feedback with two different tones and vibrational rates. It also provides drop-off warning. Mobile robotics technology has been applied to ETAs. GuideCane is a mobile robot that guides the user to their destination, while detecting and avoiding both ground obstacles and overhanging objects [13]. Stereo vision-based obstacle detection has been exploited in [8], which combines disparity measurement for obstacle detection with motion estimation and the use of an inclinometer. The Wheelchair Pathfinder combines ultrasonic and laser radar sensors mounted on a wheelchair and offers forward, side and step detection with audio and/or tactile feedback. Systems that integrate multiple technologies for travel aid have been designed. The MoBIC system [10] provides assistance in exploring maps and planning journeys, and in executing those plans by offering navigation and orientation assistance. A GPS receiver is a integral part of this system, while local navigation information is expected to come from a long cane or guide dog. The issue of standardization and integration of ETAs has been studied in [3].

Unlike sonar, laser ranging allows for a greater range of operation. Its narrower beam and shorter wavelength combine to detect finer detail necessary for shape and pattern perception. A laser ranging

device has provided range measurements for an autonomous robot [9].

Rather than object detection, for which sonar is better suited, we examine the sonification of infrared range measurements in order to perceive shapes and patterns (e.g. detection of corners, stairs, and depth discontinuities) in the user's environment. The ultimate goal of our work is to develop a device that will enable the perception of 3D space by the visually impaired user.

2 The Sonification of Range Information

The range data sonification process involves a user holding or carrying on her head a point laser ranging device that produces a stream of measurements of the range to the object, at which the laser beam is pointing at any given instant. The user can scan the environment and thereby control the direction of the laser beam. Such "interactive" use of the laser range sensor allows the user to "inspect" surrounding space and perceive its spatial properties through perception of the stream of range measurements. Sonifying the stream of range measurements is a natural way for the user to perceive it. Figure 1 illustrates the range data sonification process. The users scan their environment and obtain

Figure 1 illustrates the range data sonification process. The users scan their environment and obtain eight range measurements per second (one measurement every 125ms), with the laser range finder (LRF). Measurements are mapped to a particular feature, pitch (frequency of the audio signal), loudness (amplitude of the audio signal) or both in the audio domain. As pure tones are annoying to humans, we instead use MIDI (Musical Instrument Digital Interface) notes of different frequencies. The MIDI scale has 128 notes, and the mapping between MIDI note index m and frequency f in Hz is $f = f_0 2^{\frac{m-60}{12}}$, where $f_0 = 261.625Hz$, which corresponds to a middle 'C'. Loudness is adjusted by varying the "velocity" of the MIDI note (in MIDI terminology). Each MIDI note is output for 90ms (e.g. there is a "small gap" of silence between successive notes), using one of the 128 instruments available with the Quick Time Music Architecture (QTMA) software synthesizer.

Two modes of operation have been defined:

- (a) **Proportional mode** where the audio feature is a nonlinear function of the instantaneous value of range. More precisely, the nonlinear function is a decaying exponential mapping.
- (b) **Derivative mode**, where the audio feature is a function of the temporal derivative of range. More precisely, the change between consecutive range measurements (an approximation to mapping the derivative of range as a function of time) are mapped to the audio domain.

In the next section, we will describe the mappings in detail.

3 Proportional Mode in Range-to-Audio Mapping

Since there are no general guidelines for sonifying data [14], several different range-to-audio (or change in range to audio) mappings were experimented with. For range-to-frequency mapping, the output produced with a decaying exponential mapping was found to be the most effective as it stressed range measurements close-by, but allowed for a perceived change in frequency throughout the entire range.

Although the LRF's maximum range exceeds 100m, the maximum range for the purpose of this work was restricted to 15m with the proportional mode of operation. This restriction was placed to ensure the user is not overloaded with information and to restrict the range of notes output. For example an increase in the maximum allowable range measurement from 15m should also be followed by an increase in the range of frequencies used to ensure there is a perceived change in frequency throughout the entire range of allowable measurements.

At the other extreme, the minimum range measurement allowable was limited to $r_0 = 0.30m$ as it is used primarily for object detection/avoidance.

While in the proportional mode, a range measurement r is mapped to frequency using the relation:

$$Frequency = kc^{-a(r-r_0)} \tag{1}$$

where k = 4200 Hz, c = 2.718 = e, $a = 0.25 m^{-1}$, $r_0 = 0.30 m$ (the minimum range allowed).

The Frequency value obtained above is then mapped to the MIDI note with the closest frequency. Using this mapping allowed range measurements close to the user (e.g. small range measurements) to be mapped to higher frequencies thereby stressing their importance of objects nearby. The maximum frequency in this mapping (4200Hz) corresponds to a range measurement of 0.30m whereas the minimum frequency (106.46Hz) corresponds to a range measurement of 15m.

4 Derivative Mode in Range-to-Audio Mapping

While in the derivative mode, rather than using the range measurements themselves, the change between consecutive range measurements (an approximation to mapping the derivative of range as a function of time) are mapped to the audio domain. Although such information may not necessarily be used to locate objects, it could be used to provide greater detail about the user's surroundings. For example, depth discontinuities will easily be detected, as there will be a sudden jump in the derivative between consecutive readings. At the other extreme, flat surfaces could also be detected as the derivative between consecutive range measurements will not change (or will change slightly).

Irrespective of the user's scanning position, scanning at a faster rate will result in a more rapid change between range measurements as opposed to scanning at a slow speed.

To allow the user to discriminate between positive and negative range change, distinct signals were used for each case. Positive/negative change indicates that the current location being measured is farther away from / closer to the user relative to the last location.

Mapping parameters are as follows:

- Maximum Allowable Change in Range (r_{max}) : $\pm r_{max} = \pm 2.3m$.
- Minimum Allowable Change in Range (r_{min}) : $\pm r_{max} = \pm 0.15m$.
- Total Number of MIDI Notes Used (N): 70

The mapping itself from the change in range Dr to a MIDI note, is a piecewise linear mapping Since MIDI notes come only in integer values, the result is rounded to the nearest integer.

$$MIDI(Dr) = \begin{cases} 25 + \frac{N}{2} \frac{r_{max} - Dr}{r_{max} - r_{min}} & r_{min} < Dr < r_{max} \\ 60 & 0 < Dr < r_{min} \\ 69 & -r_{min} < Dr < 0 \\ 69 + \frac{N}{2} \frac{|Dr| - r_{min}}{r_{max} - r_{min}} & -r_{max} < Dr < -r_{min} \end{cases}$$
(2)

Several points should be made regarding this method.

- Although a linear mapping was used between range and MIDI note, adjacent notes of the musical scale differ logarithmically. As a result the change in range measurements to frequency did follow a logarithmic mapping.
- Although several of the frequencies associated with positive changes in range measurements ("Moving Away") are fairly low, and may sound displeasing when output as regular tones, generating the output using the piano instrument of the QTMA resulted in a pleasing sound

5 Testing the Accuracy and Precision of the Sonification of Range Measurements

With both modes, range measurements are mapped to frequency in the form of MIDI (Musical Instrument Digital Interface) notes. The MIDI note was output using the Quick Time Music Architecture (QTMA) software synthesizer. In particular, all notes were generated using instrument 1 - piano. Midi

notes range from 1 - 128 and follow the scale of equal temperament in which every octave (a 2:1 change in frequency) is divided into 12 equal intervals allowing for the frequency of adjacent notes to differ by a factor of 1.05946 (twelfth root of two) - e.g. adjacent keys differ logarithmically.

Information relevant to both mappings is shown in Table 1.

Range Readings per Second	8
LRF Accuracy	+/- 10cm (however, we have found this value is slightly more!!)
Headphone Volume	Adjustable
MIDI Note Duration	100ms - small gap of silence between consecutive sounds
MIDI Note Amplitude (Volume)	Constant value of 80 (max. allowable amplitude = 127)

Table 1: System parameters relevant to both mappings

5.1 Subjects

Seven females and five males (total of 12) subjects participated in the study. The age of the subjects ranged from 18 to 50, with a mean of 32. Ten of the subjects had normal vision and were blindfolded during the entire experiment. Two of the subjects were visually impaired, in that they had their eyes removed in early childhood, 2 and 3 years of age, due to retino-blastoma. All the subjects were paid for their participation.

5.2 General Method

All the experiments were conducted in an empty, spacious room (1460cm x 420cm). Each experimental session lasted for approximately three hours for the normal vision subjects and approximately five hours for the visually impaired subjects. At the beginning of the session the subjects received between 45 minutes to an hour of training on how to use the device. The training took approximately 2 hours for the visually impaired subjects. To blindfold the subjects, a pair of 'covered' ski goggles were used which prevented the subjects from viewing the experimental set-up. The subjects sat on a chair that

was pushed around by the experimenter and were holding the LRF unit with both their hands, as shown in Figure 2. The distance between a "laser dot" created by the laser pointer attached to the LRF and the feature that subjects were instructed to detect (i.e. pointing error) was measured and recorded by the experimenter. The accuracy of pointing was obtained by taking the average of pointing errors for each subject on repetitive trials. The precision of pointing was measured by the standard deviation of the repetitive pointing errors. The data was further analyzed using the Repeated Measures ANOVA [12].

5.2.1 Experiment 1: Detection of Depth Discontinuities

As illustrated in figure 3, the subjects were positioned in front (30cm to the left or right with respect to the centre of a gap) of a vertical gap at a distance of two, six and 12 metres. The gap was 20cm wide and 30cm deep. The subjects were asked to indicate the left and right edge of the gap. There were three repetitions for each edge at each of the three distances. Pointing in the direction of the gap was recorded as yielding a positive error and pointing away from the gap as negative.

The subject's accuracy (average pointing error) for the different distances for the proportional mode ranged from -0.009^o to 0.301^o and for the derivative mode from 0.025^o to 0.214^o . The precision (standard deviation of pointing error) ranged from $\pm 0.183^o$ to $\pm 0.549^o$ for the proportional mode and $\pm 0.212^o$ to $\pm 0.469^o$ for the derivative mode. For the proportional mode the overall accuracy was 0.133^o and precision $\pm 0.349^o$ and for the derivative mode 0.104 ± 0.319^o respectively. The accuracy and precision for the visually impaired subjects were -0.009 ± 0.549^o and -0.005 ± 0.304^o for the proportional mode and 0.085 ± 0.469^o and 0.056 ± 0.329^o for the derivative mode.

There were no statistically significant differences in accuracy $(F_{1,360} = 1.179, NS)$ and precision $(F_{1,72} = 0.014, NS)$ between the two modes. Figure 4 illustrates accuracy and precision for different modes and distances across all the subjects.

5.2.2 Experiment 2: Detection of Vertical and Horizontal Corners

To measure the subjects' ability to detect vertical corners, the subjects were positioned at a distance of three metres away from a corner between two walls. The task was performed from three different angular positions, i.e. 15, 30 and 45 degrees with respect to the corner (see figure 5). The subjects were never directly facing the corner; they were rotated by 15 - 20 degrees to the left or right with respect to the corner. There were five repetitions for each position tested.

To measure the subjects' ability to detect horizontal corners, the subjects were positioned at two, six, and 12 metres away from a wall and asked to point at the corner between the wall in front of them and the floor. There were five repetitions for each distance tested.

Vertical Corner. The subject's accuracy for the different angles of pointing for the proportional mode ranged from -0.771^{o} to 2.017^{o} and for the derivative mode from -7.459^{o} to 8.517^{o} . The precision ranged from $\pm 0.136^{o}$ to $\pm 2.026^{o}$ for the proportional mode and $\pm 0.334^{o}$ to $\pm 10.566^{o}$ for the derivative mode. For the proportional mode the overall accuracy was 0.747^{o} and precision $\pm 1.371^{o}$ and for the derivative mode 2.424 ± 4.355^{o} . The accuracy and precision for the visually impaired subjects were 0.239 ± 0.565^{o} and 0.815 ± 1.461^{o} for the proportional mode and -2.607 ± 3.693^{o} and 3.596 ± 3.576 for the derivative mode.

Figure 6 illustrates the accuracy and precision for the different modes and angles of pointing across all the subjects. There was a difference in accuracy between the two modes ($F_{1,22} = 5.433, p < 0.05$) with pointing using the proportional mode being more accurate than pointing using the derivative mode. Also, pointing using the derivative mode was becoming progressively less accurate with an increase in the angle of pointing ($F_{2,22} = 4.330, p < 0.05$). Similarly, pointing using the proportional mode was more precise than pointing using the derivative mode ($F_{1,22} = 19.622, p < 0.001$), and precision of pointing using the derivative mode was becoming worse as the angle of pointing increased while

precision of pointing using the proportional mode stayed the same $(F_{2,22} = 9.447, p < 0.001)$.

Horizontal Corner. The subject's accuracy for the different distances for the proportional mode ranged from -2.223° to 2.195° and for the derivative mode from -5.191° to 4.657° . The precision ranged from $\pm 0.072^{\circ}$ to $\pm 3.225^{\circ}$ for the proportional mode and $\pm 0.212^{\circ}$ to $\pm 3.577^{\circ}$ for the derivative mode. For the proportional mode the overall accuracy was 0.515° and precision $\pm 1.493^{\circ}$ and for the derivative mode $0.815 \pm 2.266^{\circ}$. The accuracy and precision for the visually impaired subjects were $-0.560 \pm 1.829^{\circ}$ and $0.791 \pm 0.91^{\circ}$ for the proportional mode and $0.915 \pm 1.064^{\circ}$ and $0.130 \pm 1.519^{\circ}$ for the derivative mode.

Figure 7 illustrates the accuracy and precision for different modes and distances of pointing across all the subjects. The accuracy of pointing did not differ between the two modes $(F_{1,22} = 1.203, NS)$. Similarly, pointing using the proportional mode was more precise than pointing using the derivative mode $(F_{1,22} = 7.785, p < 0.05)$, with precision of pointing using both the derivative and proportional mode becoming worse as the distance decreased i.e. the angle of pointing increased $(F_{2,22} = 48.456, p < 0.0001)$.

5.3 Experiment 3: Locating an Object in the Surrounding Space.

Subjects were asked to scan the surrounding space and point the LRF at the experimenter that was positioned at one of the five locations as illustrated in figure 8.

When pointing using the derivative mode seven of the 12 subjects were accurate in finding the experimenter at all the locations. Four subjects located the experimenter at four out of the five locations. One subject failed to locate the experimenter at two out of the five locations. Five out of the six misses occurred when the experimenter was located at position one and, one when the experimenter was located at position three. When pointing using the proportional mode, eight of the 12 subjects were accurate

in finding the experimenter at all the locations. Four subjects located the experimenter at four out of the five locations. All the misses occurred when the experimenter was located at position three.

6 Conclusions

Our study suggests that the sonification of range measurements is a promising approach for conveying information about spatial features. With both proportional and derivative mode the subjects were able to accurately and precisely locate depth discontinuities as well as vertical and horizontal corners. The only exception was pointing while in the derivative mode at the vertical corner from the angle of 45 degrees. Initially, the output from the proportional mode was reported as more comprehensible than the output from the derivative mode. However, after the experimental session most subjects expressed an opinion suggesting that the combination of both modes was more informative than either of the modes alone. This point is supported by the results of experiment three, where the derivative mode was superior in detection of an object closely located in front of a flat surface, while the proportional mode was more efficient in locating objects positioned in a more complex environment, with more spatial features in the background. Our data with visually impaired subjects is very preliminary. Proper clinical experiments with visually impaired subjects are required to investigate the extent to which this approach can be useful to members of that population, and to quantify the statistically significant differences, if any, in performance between visually impaired and blindfolded subjects. Future research should involve the comparison of this system with existing ETA technologies. Finally, the issue of information overload when exploring more complex environments needs to be addressed.

Acknowledgements. The work was supported by a research grant from the National Science and Engineering Council of Canada (NSERC) and an NSERC summer research scholarship to B. Kapralos. We thank Prof. Patrick Dymond for suggesting the use of MIDI, Prof. Laurence Harris for suggesting

the use of derivative mappings, and Robert Arrabito of DCIEM for his valuable comments and his encouragement. Greg Reid provided help with audio and signal processing facilities.

References

- [1] The Trisensor (KASPA TM): Wideangle untrasonic head mounted mobility aid. Technical Report http://www.sonicvision.co.nz/, SonicVisionN Ltd., 1994 (accessed on Sep. 12, 2001).
- [2] Mowat: a lightweight, hand-held, ultrasound mobility aid. Technical Report http://www.pulsedata.co.nz/, Pulsedata Co., New Zealand, (not in production) (accessed on Aug. 22, 2001).
- [3] Simon Harper. Standardising electronic travel aid interaction for visually impaired people. Technical Report http://www.man.ac.uk/towel/mphil.pdf, MPhil. thesis, Department of Computation, Univ. of Manchester Institute of Science and Technology (UMIST), 1998 (accessed on Aug. 22, 2001).
- [4] A. D. Heyes. Sonic pathfinder: A head mounted ultrasonic mobility device for outdoor use. Technical Report http://www.sonicpathfinder.org/, 1994 (accessed on Aug. 22, 2001).
- [5] Brytech Inc. Sensory 6: a navigation aid for the blind. Technical Report http://www.brytech.com/, Ottawa, Ontario, Canada, 1985-1995 (accessed on Aug. 22, 2001).
- [6] Sten Lofving. The Talking Cane: A blind people's cane, with built in radar functions. Technical Report http://www.reab.se/lofving/lhfs/, REAB Data AB, Sweden, 1994 (accessed on Aug. 22, 2001).

- [7] Peter Meijer. voice: Vision substitution technology for the blind. Technical Report http://www.seeingwithsound.com/voice.htm, Philips Research Laboratories, Eindhoven, The Netherlands, 1968 (accessed on Aug. 22, 2001).
- [8] N. Molton N, S. Se, J.M. Brady, D. Lee, and P. Probert. A Stereo vision-based aid for the visuallyimpaired. *Image and Vision Computing Journal*, 16(4):251–263, 1998.
- [9] S. B. Nickerson, P. Jasiobedzki, D. Wilkes, M. Jenkin, E. Milios, J. Tsotsos, A. Jepson, and O.N. Bains. The ARK project: Autonomous mobile robots for known industrial environments. *Robotics and Autonomous Systems*, 23(1-2):83-104, Oct. 1998.
- [10] H. Petrie, V. Johnson, T. Strothotte, A. Raab, R. Michel, L. Reichert, and A. Schalt. MoBIC: An Aid to Increase the Independent Mobility of Blind Travellers. The British Journal of Visual Impairment, 15(2), 1996.
- [11] Greg Phillips. Miniguide: Palm-held ultrasonic ranging device, with multiple modes (range sensitivy) and audio and tactile versions. Technical Report http://users.senet.com.au/~gphillip/ultra.htm, GDP Research, Adelaide, South Australia, (accessed on Aug. 22, 2001).
- [12] James Stevens. Applied Multivariate Statistics for the Social Sciences (3rd ed.). Lawrence Erlbaum Associates, Inc., Mahway NJ, 1996.
- [13] I. Ulrich and J. Borenstein. The guidecane applying mobile robot technologies to assist the visually impaired. *IEEE Transaction on Systems, Man, and Cybernetics-Part A: Systems and Humans*, 31(2):131–136, March 2001.

[14] B. Walker and G. Kramer. Mappings and metaphors in auditory displays: An experimental assessment. In Proc. of the Third International Conference on Auditory Display, Palo Alto, California, Nov. 4-6 1996.

List of Figures

1	Overview of Sonification of Range Data	16
2	Photograph of a subject during an experiment	16
3	Experiment 1 - experimental set-up. The subject positioned in front (30cm to the left or	
	right with respect to the centre of a gap) of a vertical gap at a distance of two, six and	
	12 metres. The gap was 20cm wide and 30cm deep. The subjects were asked to indicate	
	the left and right edge of the gap.	17
4	Means and standard deviations of pointing accuracy when pointing while in the propor-	
	tional (circles) or derivative (triangles) mode at the vertical gap located at two, six and	
	12 metres	18
5	Experiment 2 - experimental set-up. The subject positioned at a distance of three metres	
	away from a corner between two walls. The task was performed from three different	
	angular positions: 15, 30 and 45 degrees with respect to the corner	19
6	Means and standard deviations of pointing accuracy when pointing while in the propor-	
	tional (circles) or derivative (triangles) mode at the vertical corner.	20
7	Means and standard deviations of pointing accuracy when pointing while in the propor-	
	tional (circles) or derivative (triangles) mode at the horizontal corner	21
8	Experiment 3 - experimental set-up. The subject scanned the surrounding space and	
	pointed the LRF at the experimenter that was positioned at one of the five locations	22

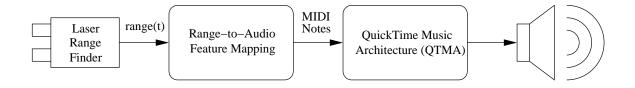


Figure 1: Overview of Sonification of Range Data.

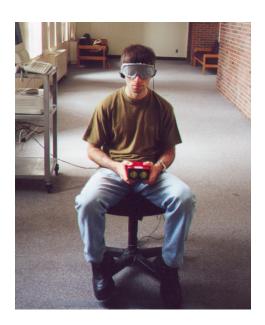


Figure 2: Photograph of a subject during an experiment.

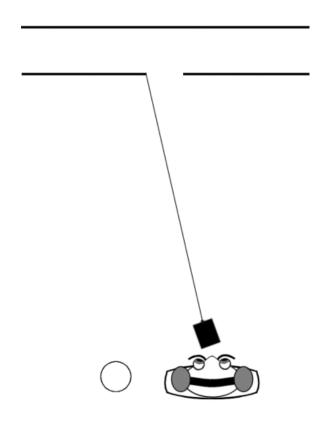


Figure 3: Experiment 1 - experimental set-up. The subject positioned in front (30cm to the left or right with respect to the centre of a gap) of a vertical gap at a distance of two, six and 12 metres. The gap was 20cm wide and 30cm deep. The subjects were asked to indicate the left and right edge of the gap.

Pointing Accuracy [deg]

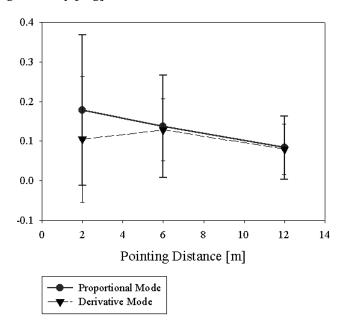


Figure 4: Means and standard deviations of pointing accuracy when pointing while in the proportional (circles) or derivative (triangles) mode at the vertical gap located at two, six and 12 metres.

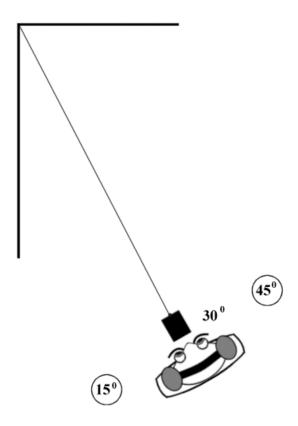


Figure 5: Experiment 2 - experimental set-up. The subject positioned at a distance of three metres away from a corner between two walls. The task was performed from three different angular positions: 15, 30 and 45 degrees with respect to the corner.

Pointing Accuracy [deg] 10 8 6 4 2 0 15 Pointing Angle [deg] Proportional Mode Derivative Mode

Figure 6: Means and standard deviations of pointing accuracy when pointing while in the proportional (circles) or derivative (triangles) mode at the vertical corner.

Pointing Accuracy [deg] 4 ______

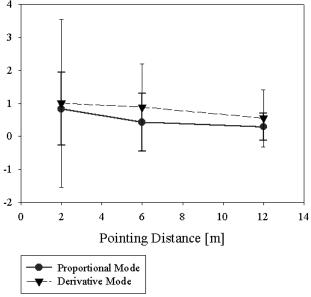


Figure 7: Means and standard deviations of pointing accuracy when pointing while in the proportional (circles) or derivative (triangles) mode at the horizontal corner.

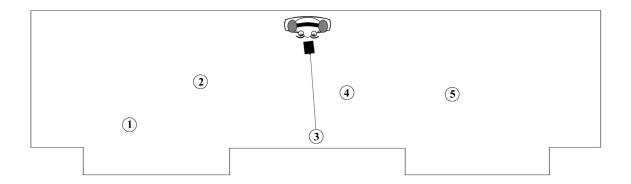


Figure 8: Experiment 3 - experimental set-up. The subject scanned the surrounding space and pointed the LRF at the experimenter that was positioned at one of the five locations.